

# Lecture 12

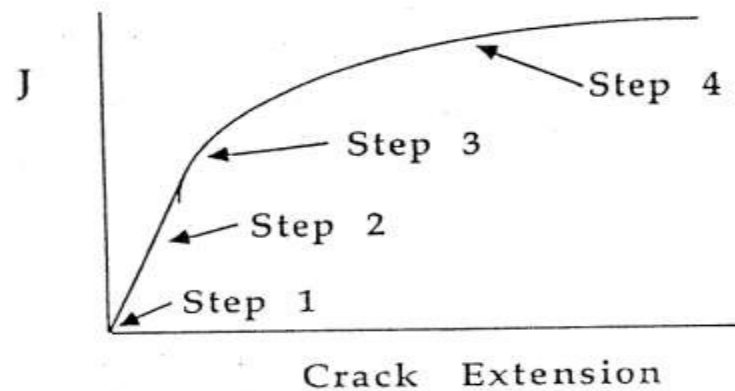
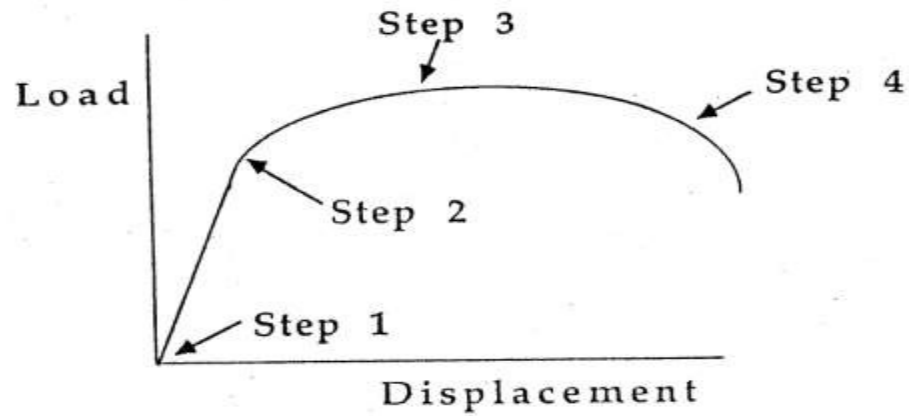
## Ductile Fracture Testing

# Ductile fracture toughness

- 1 Ductile fracture is a mechanism of failure in a material which occurs by the initiation, growth and coalescence of voids
- 2 Ductile fracture is a process rather than an event; therefore it is better characterized by a curve than a single point
- 3 The curve is a plot of a fracture parameter versus crack extension, called the crack growth resistance curve or R curve
- 4 J or CTOD,  $\delta$ , are the fracture parameters used

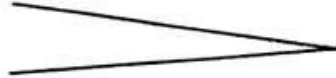
## Ductile Fracture Process

Load vs Displacement and  $J$  vs  $\Delta a$



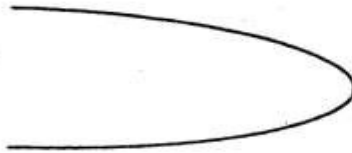
## Ductile Fracture Process

Step 1



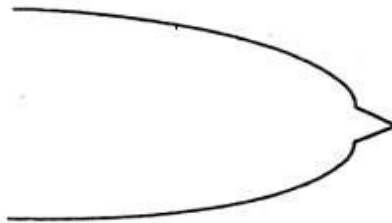
No Load:  
Sharp Crack

Step 2



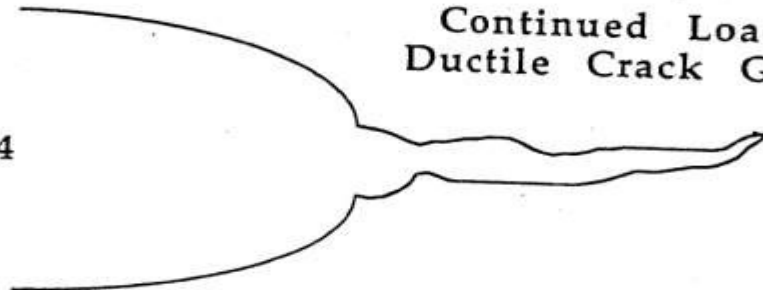
Loading:  
Crack Blunting

Step 3



More Loading:  
Ductile Initiation

Step 4



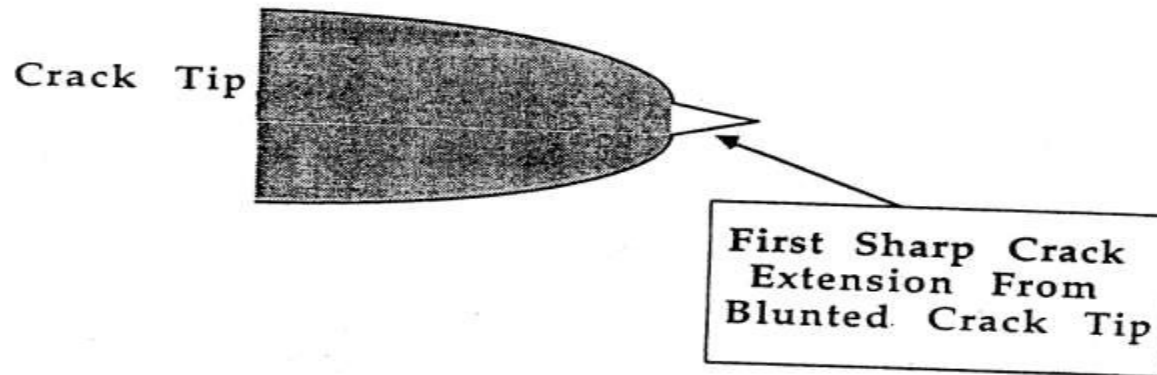
Continued Loading:  
Ductile Crack Growth

# Concept of crack initiation in ductile fracture

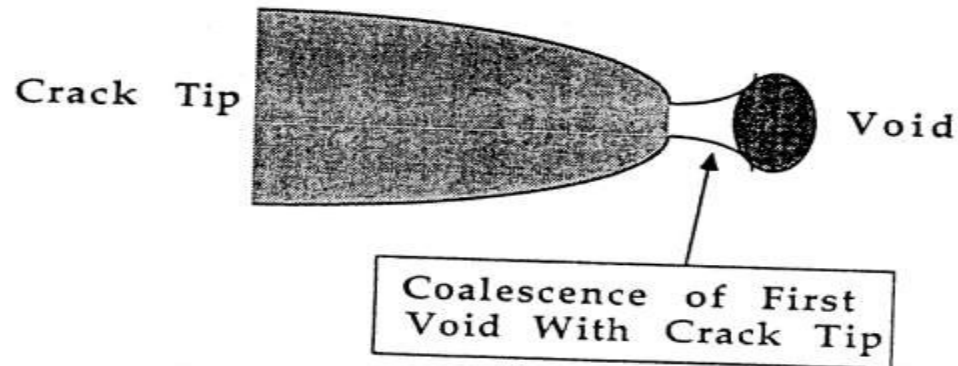
1.  $J_{Ic}$  is the value of fracture toughness near the initiation of slow, stable crack growth for metallic materials
2. The concept of the first point of initiation versus an engineering estimate, analogy to the tensile test,  $\sigma_{ys}$
3.  $J$  is determined from a J-R curve using a set of construction and analysis rules

## Concept of ductile fracture initiation

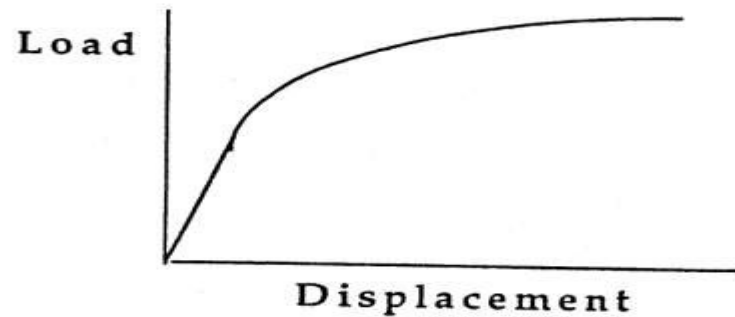
### Macro-mechanics View



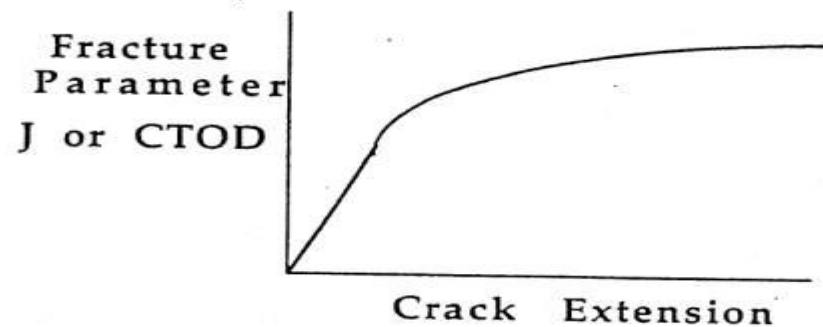
### Micro-mechanics View



## Goal of ductile fracture toughness test



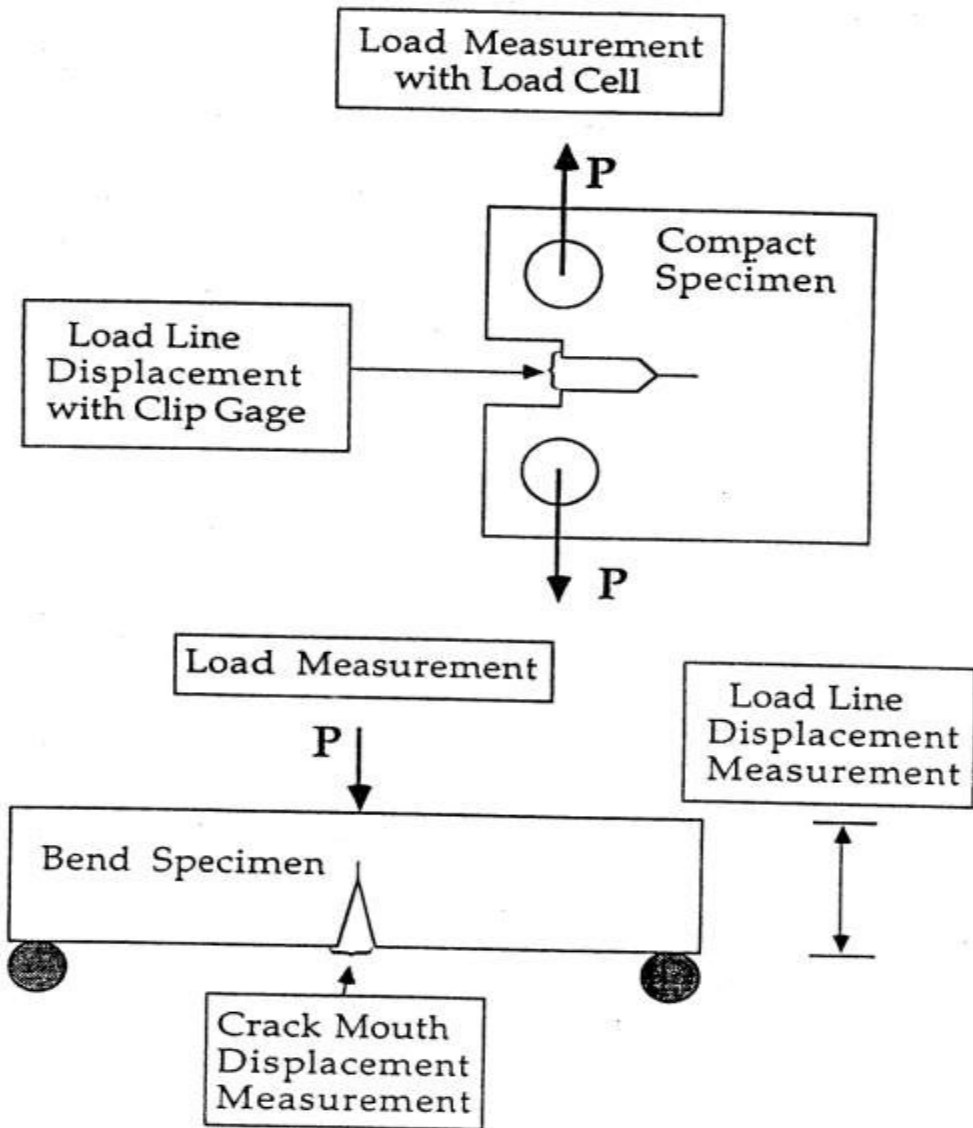
1. Test fracture toughness specimen to get load versus displacement data
2. Analyze data to get plot of fracture parameter versus crack extension



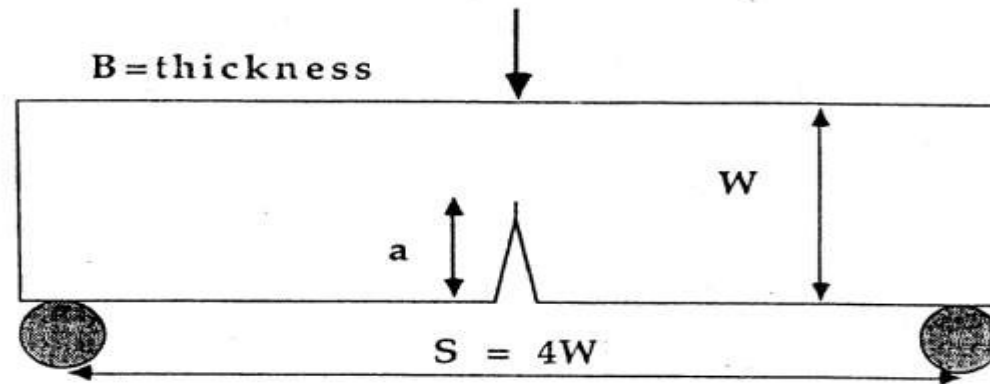
# Basic need for a ductile fracture toughness test

- 1 Load versus displacement data with a measurement of crack extension
- 2 Formulas to calculate the fracture parameters; J or CTOD
- 3 Special plotting of construction if an initiation point is desired
- 4 Qualification or validity requirements

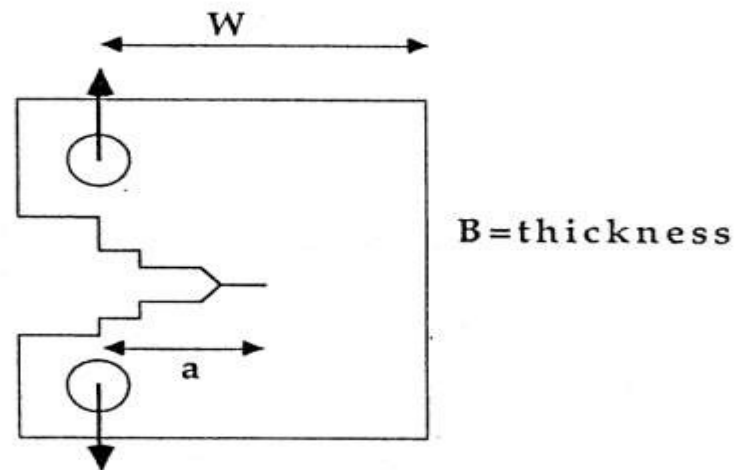
# Fracture Toughness Test Parameters



## Fracture toughness test specimens



Single Edge Notched Bend Specimen  
with Three Point Loading

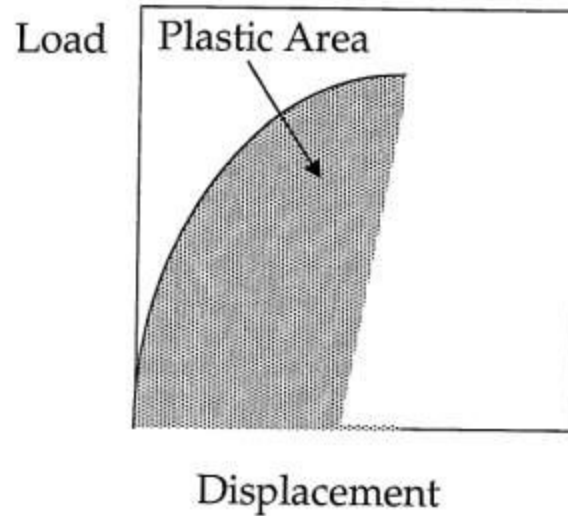


Compact Specimen  
with Pin and Clevis Loading

## J Formulas for $J_{Ic}$ test

1.  $J = J_{el} + J_{pl}$

$$J = \frac{K^2(1-\nu^2)}{E} + \frac{\eta_{pl}Area}{Bb}$$



$$\eta_{pl} = 2.0 \quad \text{bend specimen}$$

$$\eta_{pl} = 2.0 + 0.522 \frac{b}{W} \quad \text{compact specimen}$$

## E 813 $J_{Ic}$ multiple specimen test

1. Specimen type CT or Bend
2. Precrack
3. Load several specimen to a range of displacements
4. Calculate  $J = J_{el} + J_{pl}$

$$J_{el} = K^2(1 - \nu^2)/E$$

$$J_{pl} = \frac{\eta_{pl}}{B b} \int_0^{v_{pl}} P dv_{pl}$$

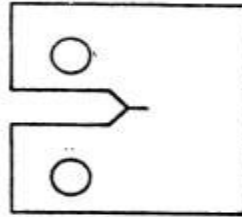
where

$$\eta_{pl} = 2, \text{ bend}$$

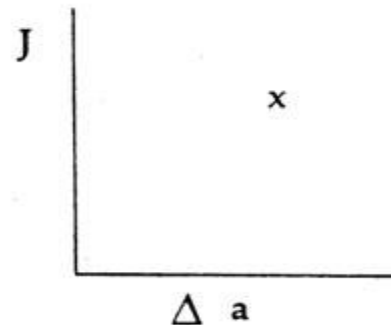
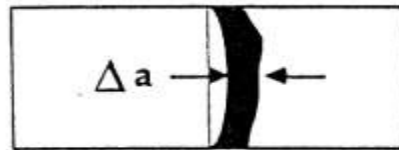
$$\eta_{pl} = 2 + 0.522 b/W, \text{ CT}$$

5. Hint tint and measure  $\Delta a$  with 9 point average
6. Plot and construct to measure  $J_{Ic}$

## Multiple Specimen $J_{Ic}$ Test

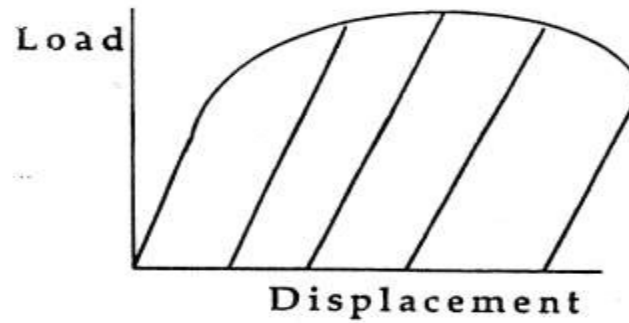


1. Start with Precracked Test Specimen
2. Generated Load vs Displacement Plot
3. Heat tint to mark crack and break open
4. Calculate  $J$  from load and displacement

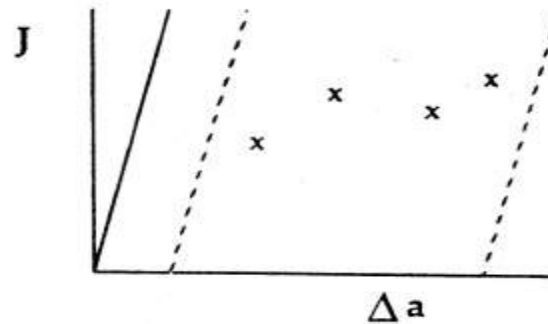


5. Measure Crack Extension Nine Point Average
6. Plot Single Point on  $J$  vs  $\Delta a$  Curve

## Multiple Specimen $J_{Ic}$ test (cont)



7. Test four or more specimens and analyze like the first one



8. Plot all  $J$  vs  $\Delta a$  Points and do  $J_{Ic}$  Construction

## **$J_{Ic}$ construction**

1. Consider only points falling between exclusion lines, need four or more points

i) Blunting line is construction line,

$$J = 2 \sigma_Y \Delta a$$

ii) Exclusion lines offset 0.15 and 1.5 mm (0.006 and 0.06 in) , same slope as construction lines

2. Top limit is  $J_{max} = (b, B)\sigma_Y/15$

3. Fit points with a power law

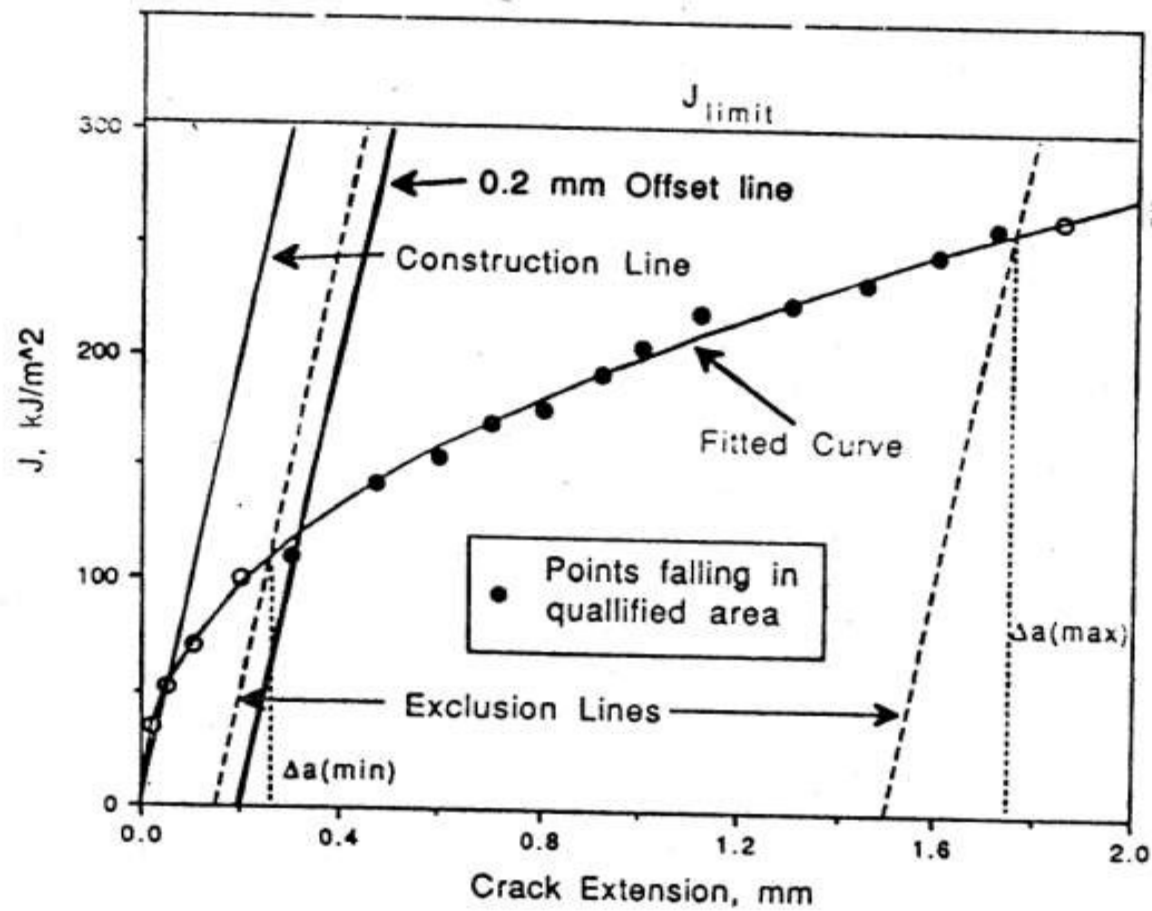
$$J = C_1 (\Delta a)^{C_2}$$

can use,

$$\ln J = \ln C_1 + C_2 \ln(\Delta a)$$

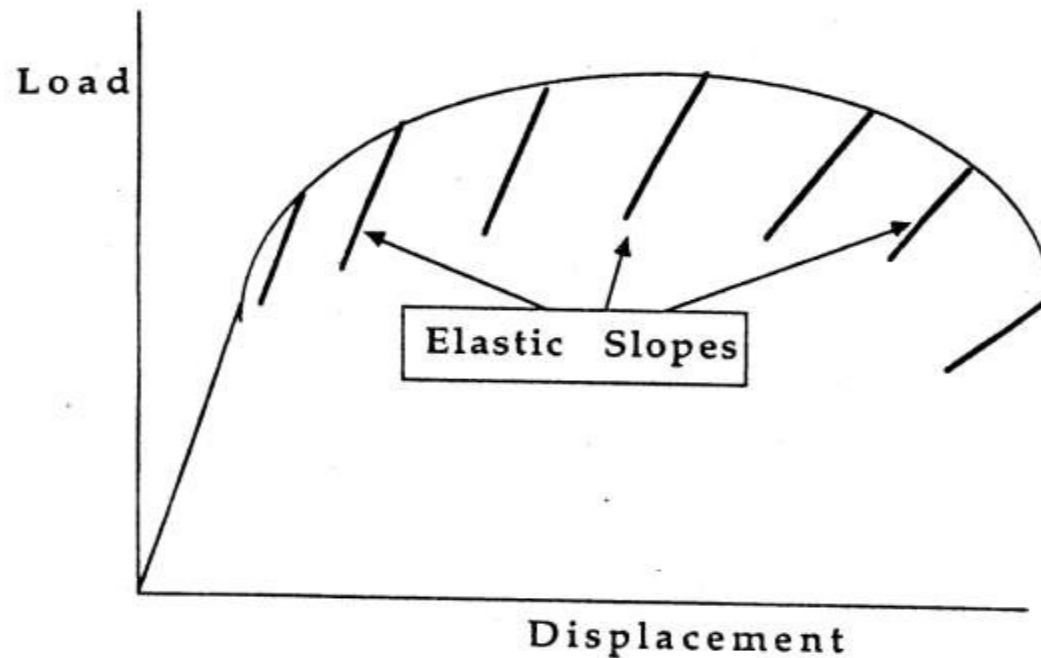
with a least square fit

4.  $J_Q$  is at the intercept of the fitted line and a 0.2 mm (.008 in) offset to the blunting line
5.  $J_Q$  is  $J_{Ic}$  if  $B, b \geq 25 J_Q/\sigma_Y$

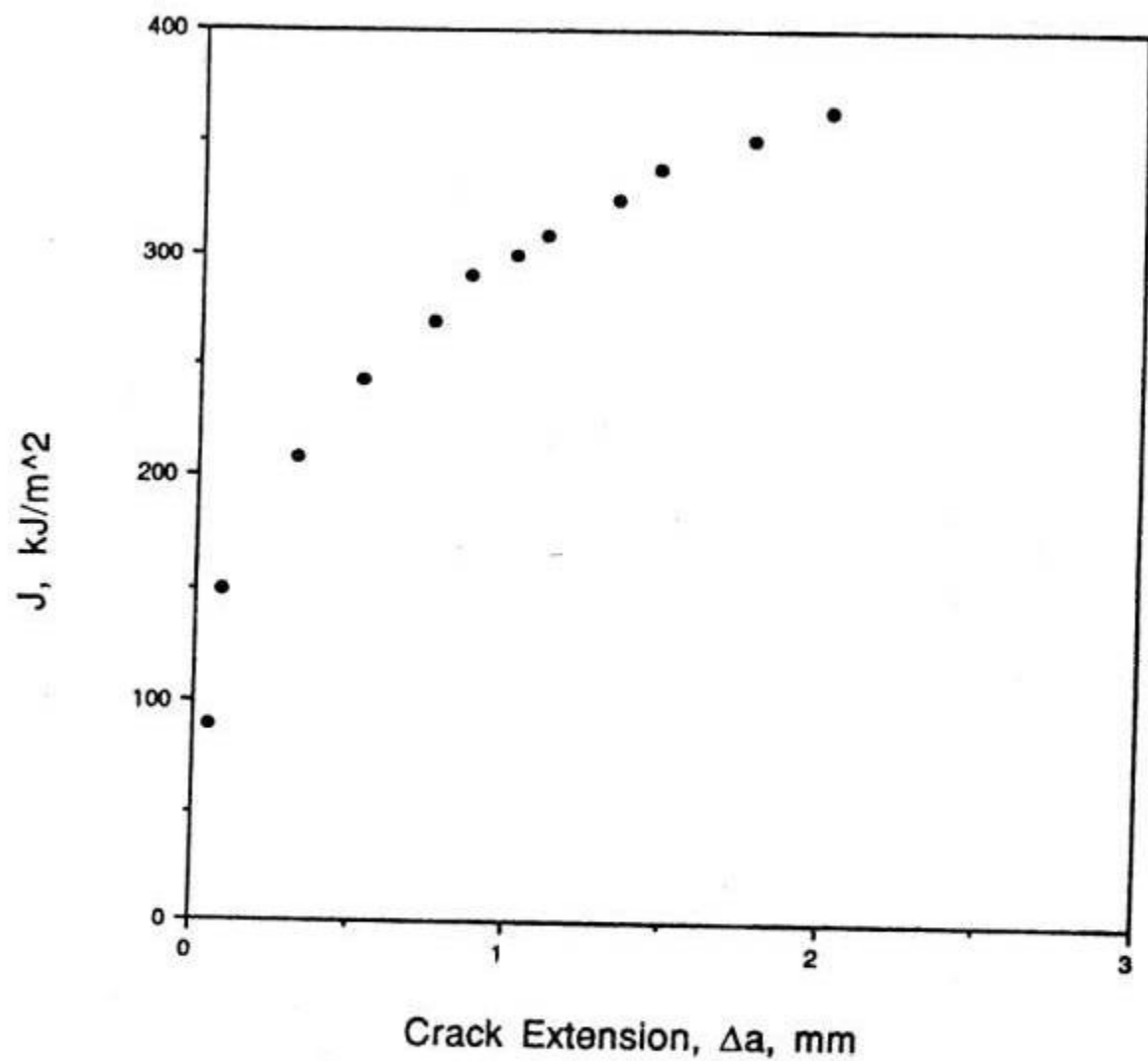


J<sub>Ic</sub> Construction plot

## Elastic Unloading Compliance



1. Elastic Slope is a measure of crack length
2. At each unload  $J$  and  $\Delta a$  can be determined
3.  $J$  versus  $\Delta a$  points are plotted and analyzed for  $J_{Ic}$  like the multiple specimen test



**Fig. 4b - Typical J-R Curve**



# Standard Test Method for Measurement of Fracture Toughness<sup>1</sup>

This standard is issued under the fixed designation E 1820; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon ( $\epsilon$ ) indicates an editorial change since the last revision or reapproval.

## 1. Scope

1.1 This test method covers procedures and guidelines for the determination of fracture toughness of metallic materials using the following parameters:  $K$ ,  $J$ , and CTOD ( $\delta$ ). Toughness can be measured in the  $R$ -curve format or as a point value. The fracture toughness determined in accordance with this test method is for the opening mode (Mode I) of loading.

1.2 The recommended specimens are single-edge bend, [SE(B)], compact, [C(T)], and disk-shaped compact, [DC(T)]. All specimens contain notches that are sharpened with fatigue cracks.

1.2.1 Specimen dimensional (size) requirements vary according to the fracture toughness analysis applied. The guidelines are established through consideration of material toughness, material flow strength, and the individual qualification requirements of the toughness value per values sought.

1.3 The values stated in SI units are to be regarded as the standard. The values given in parentheses are for information only.

1.4 This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.

NOTE 1—Other standard methods for the determination of fracture toughness using the parameters  $K$ ,  $J$ , and CTOD are contained in Test Methods E 399, E 813, E 1152, E 1290, and E 1737. This test method was developed to provide a common method for determining all applicable toughness parameters from a single test.

## 2. Referenced Documents

### 2.1 ASTM Standards:

- E 4 Practices for Force Verification of Testing Machines<sup>2</sup>
- E 8 Test Methods for Tension Testing of Metallic Materials<sup>2</sup>
- E 21 Test Methods for Elevated Temperature Tension Tests of Metallic Materials<sup>2</sup>
- E 399 Test Method for Plane-Strain Fracture Toughness of Metallic Materials<sup>2</sup>

<sup>1</sup> This test method is under the jurisdiction of ASTM Committee E-8 on Fatigue and Fracture and is the direct responsibility of Subcommittee E08.08 on Elastic-Plastic Fracture Mechanics Technology.

Current edition approved January 10, 1999. Published July 1999. Originally published as E 1820 - 96. Last previous edition E 1820 - 98.

<sup>2</sup> Annual Book of ASTM Standards, Vol 03.01.

E 813 Test Method for  $J_{Ic}$ , A Measure of Fracture Toughness<sup>2</sup>

E 1152 Test Method for Determining  $J$ - $R$  Curves<sup>2</sup>

E 1290 Test Method for Crack-Tip Opening Displacement (CTOD) Fracture Toughness Measurement<sup>2</sup>

E 1737 Test Method for  $J$ -Integral Characterization of Fracture Toughness<sup>2</sup>

E 1823 Terminology Relating to Fatigue and Fracture Testing<sup>2</sup>

## 3. Terminology

3.1 Terminology E 1823 is applicable to this test method.

### 3.2 Definitions:

3.2.1 *compliance* [ $LF^{-1}$ ],  $n$ —the ratio of displacement increment to load increment.

3.2.2 *crack displacement* [ $L$ ],  $n$ —the separation vector between two points (on the surfaces of a deformed crack) that were coincident on the surfaces of an ideal crack in the undeformed condition.

3.2.2.1 *Discussion*—In this practice, displacement,  $v$ , is the total displacement measured by clip gages or other devices spanning the crack faces.

3.2.3 *crack extension*,  $\Delta a$  [ $L$ ],  $n$ —an increase in crack size.

3.2.4 *crack-extension force*,  $G$  [ $FL^{-1}$  or  $FLL^{-2}$ ],  $n$ —the elastic energy per unit of new separation area that is made available at the front of an ideal crack in an elastic solid during a virtual increment of forward crack extension.

3.2.5 *crack size*,  $a$  [ $L$ ],  $n$ —a lineal measure of a principal planar dimension of a crack. This measure is commonly used in the calculation of quantities descriptive of the stress and displacement fields, and is often also termed crack length or depth.

3.2.5.1 *Discussion*—In practice, the value of  $a$  is obtained from procedures for measurement of physical crack size,  $a_p$ , original crack size,  $a_o$ , and effective crack size,  $a_e$ , as appropriate to the situation being considered.

3.2.6 *crack-tip opening displacement (CTOD)*,  $\delta$  [ $L$ ],  $n$ —the crack displacement due to elastic and plastic deformation at variously defined locations near the original (prior to an application of load) crack tip.

3.2.6.1 *Discussion*—In this test method, CTOD is the displacement of the crack surfaces normal to the original (unloaded) crack plane at the tip of the fatigue precrack,  $a_o$ . In this test method, CTOD is calculated at the original crack length,

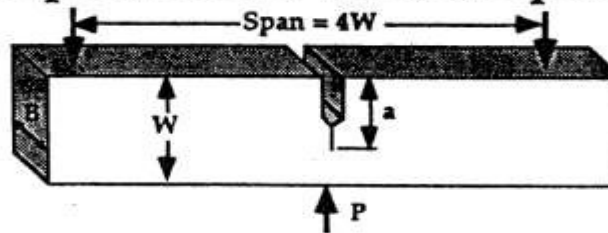
# Latest Combined Standard

- **ASTM E1820 - 08a Standard Test Method for Measurement of Fracture Toughness**

## CTOD TESTING (ASTM E 1290-89)

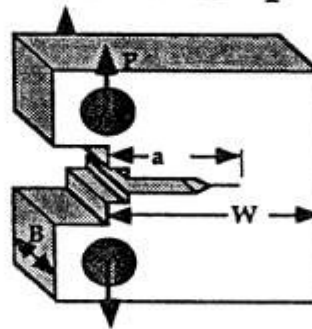
### A. Specimen Configurations and Dimensions

Three-point bend [SE(B)] specimen:



$$0.45 \leq a_0/W \leq 0.55$$
$$W/B = 1 \text{ or } 2$$

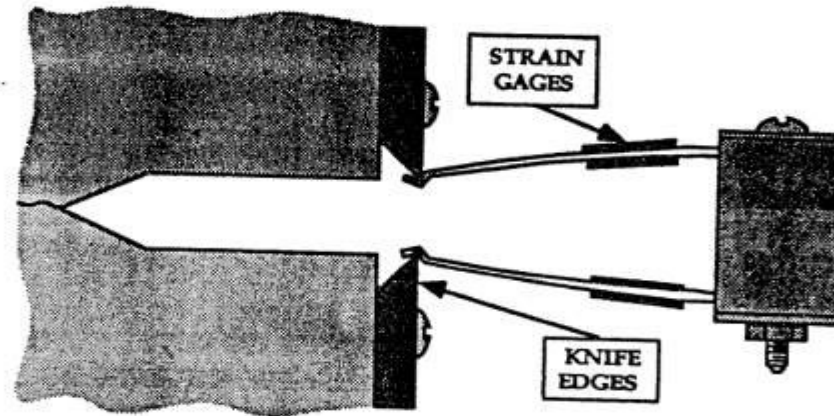
Compact [C(T)] specimen:



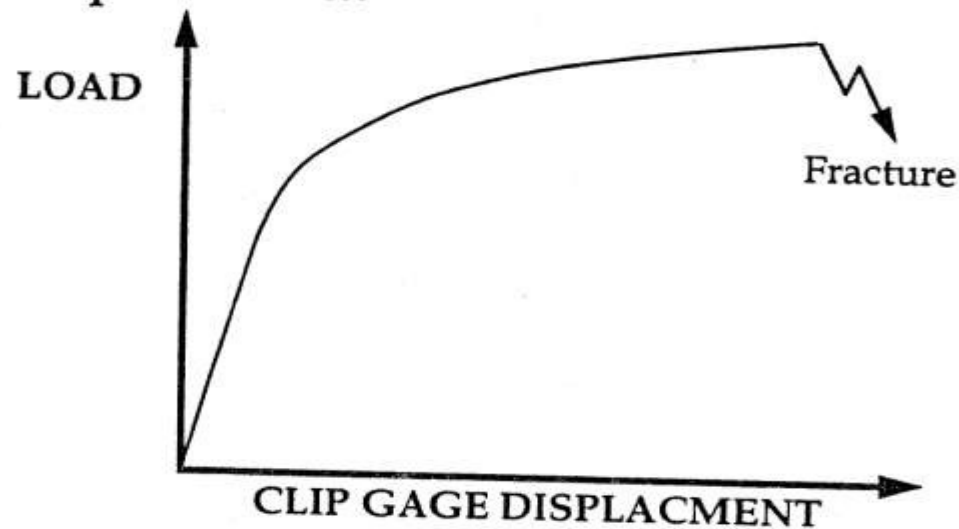
$$0.45 \leq a_0/W \leq 0.55$$
$$2 \leq W/B \leq 4$$

## B. Instrumentation

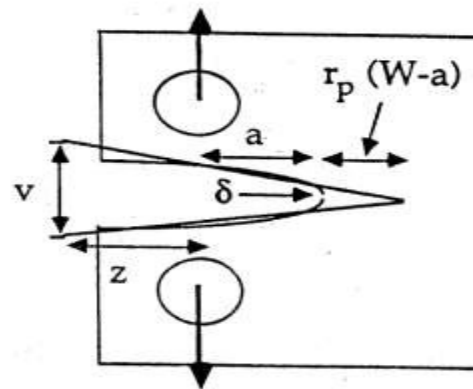
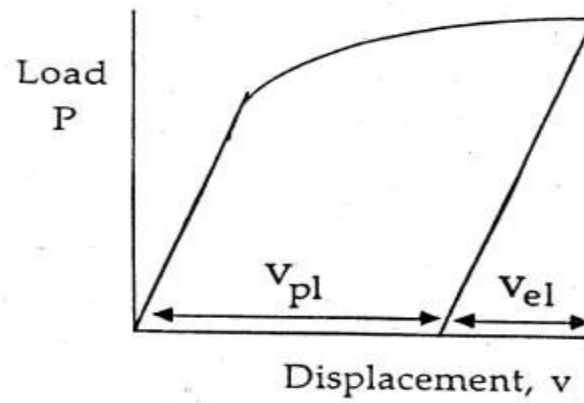
Clip gage displacement measured at the mouth of the crack:



Load is plotted versus clip gage displacement:



## CTOD Equations



$$\delta = \delta_{el} + \delta_{pl}$$

$$= \frac{K^2(1-\nu^2)}{2 \sigma_{ys} E} + \frac{r_p(W-a)v_{pl}}{r_p(W-a) + a + z}$$

$$r_p = 0.4(1 + \alpha)$$

For a bend specimen:

$$\alpha = 0.10$$

$$r_p = 0.44$$

For a compact specimen:

$$\alpha = 2 \left[ \left( \frac{a_o}{b_o} \right)^2 + \frac{a_o}{b_o} + 0.5 \right]^{1/2} - 2 \left[ \frac{a_o}{b_o} + 0.5 \right]$$

where  $b_o = W - a_o$

$$r_p \approx 0.47 \text{ for } 0.45 \leq a_o/W \leq 0.50$$

and

$$r_p \approx 0.46 \text{ for } 0.50 < a_o/W \leq 0.55$$

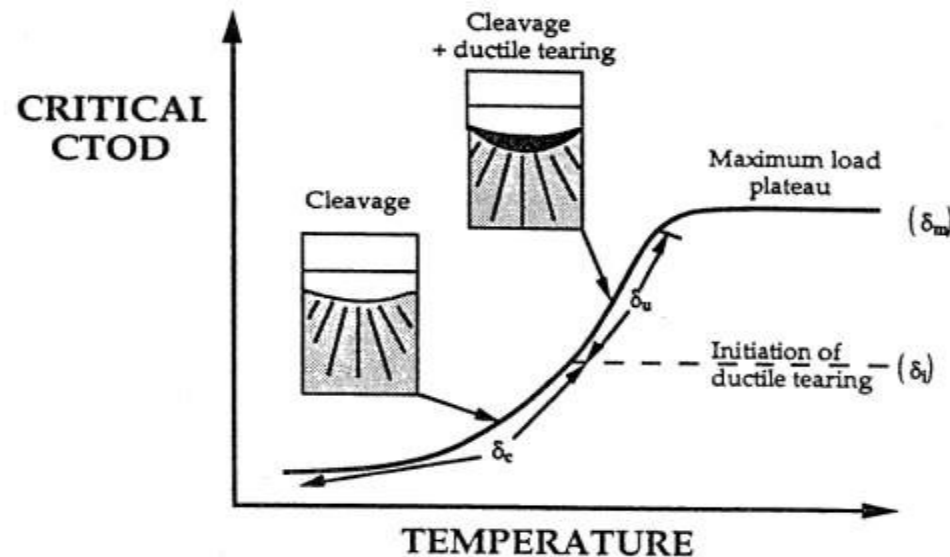
## D. Notation for Critical CTOD Values

$\delta_c$  - Critical CTOD at the onset of unstable fracture without prior stable crack growth.

$\delta_u$  - Critical CTOD at the onset of unstable fracture which has been preceded by stable crack growth.

$\delta_i$  - CTOD at the initiation of stable crack growth.

$\delta_m$  - CTOD at the maximum load plateau.





# Standard Test Method for Crack-Tip Opening Displacement (CTOD) Fracture Toughness Measurement<sup>1</sup>

This standard is issued under the fixed designation E 1290; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon ( $\epsilon$ ) indicates an editorial change since the last revision or reapproval.

## 1. Scope

1.1 This test method covers the determination of critical crack-tip opening displacement (CTOD) values at one or more of several crack extension events. These CTOD values can be used as measures of fracture toughness for metallic materials, and are especially appropriate to materials that exhibit a change from ductile to brittle behavior with decreasing temperature. This test method applies specifically to notched specimens sharpened by fatigue cracking. The recommended specimens are three-point bend [SE(B)] or compact [C(T)] specimens. The loading rate is slow and influences of environment (other than temperature) are not covered. The specimens are tested under crosshead or clip gage displacement controlled loading.

1.1.1 The recommended specimen thickness,  $B$ , is that of the material in thicknesses intended for an application. Superficial surface machining may be used when desired.

1.1.2 For the recommended three-point bend specimens [SE(B)], width,  $W$ , is either equal to, or twice, the specimen thickness,  $B$ , depending upon the application of the test. (See 4.3 for applications of the recommended specimens.) For SE(B) specimens the recommended initial normalized crack size is  $0.45 \leq a_0/W \leq 0.55$ . The span-to-width ratio ( $S/W$ ) is specified as 4.

1.1.3 For the recommended compact specimen [C(T)] the initial normalized crack size is  $0.45 \leq a_0/W \leq 0.55$ . The half-height-to-width ratio ( $H/W$ ) equals 0.6 and the width to thickness ratio is within the range  $2 \leq W/B \leq 4$ .

1.2 This standard does not purport to address all of the safety problems, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.

## 2. Referenced Documents

- 2.1 *ASTM Standards*:
- E 4 Practices for Force Verification of Testing Machines<sup>2</sup>
- E 8 Test Methods for Tension Testing of Metallic Materials<sup>2</sup>
- E 399 Test Method for Plane-Strain Fracture Toughness of Metallic Materials<sup>2</sup>
- E 616 Terminology Relating to Fracture Testing<sup>2</sup>

<sup>1</sup> This test method is under the jurisdiction of ASTM Committee E-8 on Fatigue and Fracture and is the direct responsibility of Subcommittee E8.08 on Elastic-Plastic Fracture Mechanics Technology.

Current edition approved March 15, 1993. Published May 1993. Originally published as E 1290 - 89. Last previous edition E 1290 - 89 $\epsilon$ 1.

<sup>2</sup> Annual Book of ASTM Standards, Vol 03.01.

E 813 Test Method for  $J_{Ic}$ , A Measure of Fracture Toughness<sup>2</sup>

E 1152 Test Method for Determining J-R Curves<sup>2</sup>

## 3. Terminology

3.1 Terminology E 616 is applicable to this test method.

3.2 *Definitions*:

3.2.1 *crack tip opening displacement, (CTOD),  $\delta[L]$* —the crack displacement due to elastic and plastic deformation at various defined locations near the original (prior to an application of load) crack tip.

*Discussion*—In this test method, CTOD is the displacement of the crack surfaces normal to the original (unloaded) crack plane at the tip of the fatigue precrack,  $a_p$ .

In CTOD testing,  $\delta_u[L]$  is the value of CTOD at the onset of unstable brittle crack extension (see 3.2.13) or pop-in (see 3.2.7) when  $\Delta a_p < 0.2$  mm (0.008 in.). The load  $P_u$  and the clip gage displacement  $v_u$  for  $\delta_u$  are indicated in Fig. 1.

In CTOD testing,  $\delta_m[L]$  is the value of CTOD at the onset of unstable brittle crack extension (see 3.2.13) or pop-in (see 3.2.7) when the event is preceded by  $\Delta a_p > 0.2$  mm (0.008 in.). The load  $P_m$  and the clip gage displacement  $v_m$  for  $\delta_m$  are indicated in Fig. 1.

In CTOD testing,  $\delta_{max}[L]$  is the value of CTOD at the first attainment of a maximum load plateau for fully plastic behavior. The load  $P_{max}$  and the clip gage displacement  $v_{max}$  for  $\delta_{max}$  are indicated in Fig. 1.

3.2.2 *effective yield strength,  $\sigma_Y [FL^{-2}]$* —an assumed value of uniaxial yield strength that represents the influence of plastic yielding upon fracture test parameters.

*Discussion*—The calculation of  $\sigma_Y$  is the average of the 0.2 % offset yield strength ( $\sigma_{YS}$ ), and the ultimate tensile strength ( $\sigma_{TS}$ ), that is  $(\sigma_{YS} + \sigma_{TS})/2$ . Both  $\sigma_{YS}$  and  $\sigma_{TS}$  are determined in accordance with Test Methods E 8.

3.2.3 *original crack size,  $a_0 [L]$* —see Terminology E 616.

3.2.4 *original uncracked ligament,  $b_0 [L]$* —the distance from the original crack front to the back surface of the specimen at the start of testing,  $b_0 = W - a_0$ .

3.2.5 *physical crack extension,  $\Delta a_p [L]$* —an increase in physical crack size,  $\Delta a_p = a_p - a_0$ .

3.2.6 *physical crack size,  $a_p [L]$* —see Terminology E 616.

*Discussion*—In CTOD testing,  $a_p = a_0 + \Delta a_p$ .

3.2.7 *pop-in*—a discontinuity in the load versus clip gage displacement record. The record of a pop-in shows a sudden increase in displacement and, generally, a decrease in load. Subsequently, the displacement and load increase to above their respective values at pop-in.

3.2.8 *slow stable crack extension  $[L]$* —a displacement controlled crack extension beyond the stretch zone width (see 3.2.12). The extension stops when the applied displacement is held constant.

3.2.9 *specimen span,  $S [L]$* —the distance between spec-

# Latest CTOD Standard

- **ASTM E1290 - 08 Standard Test Method for Crack-Tip Opening Displacement (CTOD) Fracture Toughness Measurement**

# Choices in fracture characterization

## 1 Deformation behavior

- Linear-elastic versus elastic plastic
- Determines fracture parameter

## 2 Fracture behavior

- Ductile versus brittle
- Determines type of fracture

## 3 Constraint

- Plane strain versus plane stress
- Determines fracture toughness values

# Matrix of Deformation versus Fracture Behavior

|                             | <b>Fracture Behavior</b> |                                     |
|-----------------------------|--------------------------|-------------------------------------|
| <b>Deformation Behavior</b> | Brittle                  | Ductile                             |
| Linear Elastic              | $K_{Ic}$                 | $K_{Ic}$<br>K-R curve               |
| Elastic-Plastic             | $J_c$ $\delta_c$         | $J_{Ic}$<br>J-R curve<br>$\delta_m$ |

## Common Test Methods

A. ASTM has 5 major test methods

E 399 -  $K_{Ic}$

E 561 - K - R curve

E 813 -  $J_{Ic}$

E 1152 - J - R curve

E 1290 - CTOD

Other special interest ones, not mentioned here

B. Problem with 5 Similar Specimens and Goals

Different details that make them exclusive

Examples:  $K_{Ic}$  test

$J_{Ic}$  test

C. Common Test Method Test Philosophy

1. Run single specimen type, single procedure
2. Let material choose type of result
3. Allow measurement of toughness in terms of K, J or d, whichever is appropriate

#### D. Test Details

1. Specimens: C(T), SEN(B), DC(T)
2. Fracture type: Fracture instability or stable tearing
3. Approach:
  - a) Run test to get  $P$ ,  $v$ ,  $a$  pairs  
(Compliance or electrical potential)
  - b) Continue test until there is a fracture instability or enough  $\Delta a$  to analyze
  - c) Evaluate all possible fracture parameters
4. Examples
  - a) Instability before  $\Delta a$ ,  $J_c$  or  $\delta_c$
  - b) Instability after  $\Delta a$ ,  $J_u$  or  $\delta_u$
  - c) No instability  $J$  or  $d$  vs  $\Delta a$  R curve, can evaluate  $J_{Ic}$  or  $\delta_{Ic}$
5. Validity now called qualified or size insensitive



## Standard Test Method for Measurement of Fracture Toughness<sup>1</sup>

This standard is issued under the fixed designation E 1820; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reappraisal. A superscript epsilon ( $\epsilon$ ) indicates an editorial change since the last revision or reappraisal.

### 1. Scope

1.1 This test method covers procedures and guidelines for the determination of fracture toughness of metallic materials using the following parameters:  $K$ ,  $J$ , and CTOD ( $\delta$ ). Toughness can be measured in the  $R$ -curve format or as a point value. The fracture toughness determined in accordance with this test method is for the opening mode (Mode I) of loading.

1.2 The recommended specimens are single-edge bend, [SE(B)], compact, [C(T)], and disk-shaped compact, [DC(T)]. All specimens contain notches that are sharpened with fatigue cracks.

1.2.1 Specimen dimensional (size) requirements vary according to the fracture toughness analysis applied. The guidelines are established through consideration of material toughness, material flow strength, and the individual qualification requirements of the toughness value per values sought.

1.3 The values stated in SI units are to be regarded as the standard. The values given in parentheses are for information only.

1.4 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.*

NOTE 1—Other standard methods for the determination of fracture toughness using the parameters  $K$ ,  $J$ , and CTOD are contained in Test Methods E 399, E 813, E 1152, E 1290, and E 1737. This test method was developed to provide a common method for determining all applicable toughness parameters from a single test.

### 2. Referenced Documents

#### 2.1 ASTM Standards:

- E 4 Practices for Force Verification of Testing Machines<sup>2</sup>
- E 8 Test Methods for Tension Testing of Metallic Materials<sup>2</sup>
- E 21 Test Methods for Elevated Temperature Tension Tests of Metallic Materials<sup>2</sup>
- E 399 Test Method for Plane-Strain Fracture Toughness of Metallic Materials<sup>2</sup>

<sup>1</sup> This test method is under the jurisdiction of ASTM Committee E-8 on Fatigue and Fracture and is the direct responsibility of Subcommittee E08.08 on Elastic-Plastic Fracture Mechanics Technology.

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<sup>2</sup> Annual Book of ASTM Standards, Vol 03.01.

E 813 Test Method for  $J_{Ic}$ , A Measure of Fracture Toughness<sup>2</sup>

E 1152 Test Method for Determining  $J$ - $R$  Curves<sup>2</sup>

E 1290 Test Method for Crack-Tip Opening Displacement (CTOD) Fracture Toughness Measurement<sup>2</sup>

E 1737 Test Method for J-Integral Characterization of Fracture Toughness<sup>2</sup>

E 1823 Terminology Relating to Fatigue and Fracture Testing<sup>2</sup>

### 3. Terminology

3.1 Terminology E 1823 is applicable to this test method.

#### 3.2 Definitions:

3.2.1 *compliance* [ $LF^{-1}$ ],  $n$ —the ratio of displacement increment to load increment.

3.2.2 *crack displacement* [ $L$ ],  $n$ —the separation vector between two points (on the surfaces of a deformed crack) that were coincident on the surfaces of an ideal crack in the undeformed condition.

3.2.2.1 *Discussion*—In this practice, displacement,  $v$ , is the total displacement measured by clip gages or other devices spanning the crack faces.

3.2.3 *crack extension*,  $\Delta a$  [ $L$ ],  $n$ —an increase in crack size.

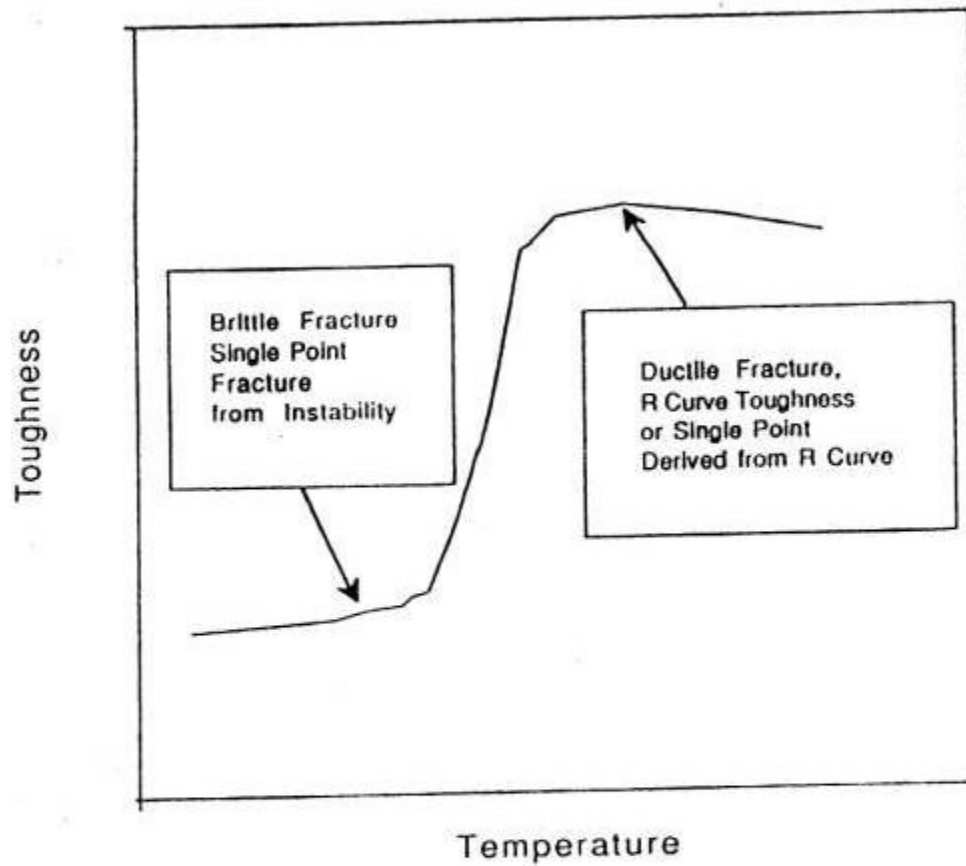
3.2.4 *crack-extension force*,  $G$  [ $FL^{-1}$  or  $FLL^{-2}$ ],  $n$ —the elastic energy per unit of new separation area that is made available at the front of an ideal crack in an elastic solid during a virtual increment of forward crack extension.

3.2.5 *crack size*,  $a$  [ $L$ ],  $n$ —a lineal measure of a principal planar dimension of a crack. This measure is commonly used in the calculation of quantities descriptive of the stress and displacement fields, and is often also termed crack length or depth.

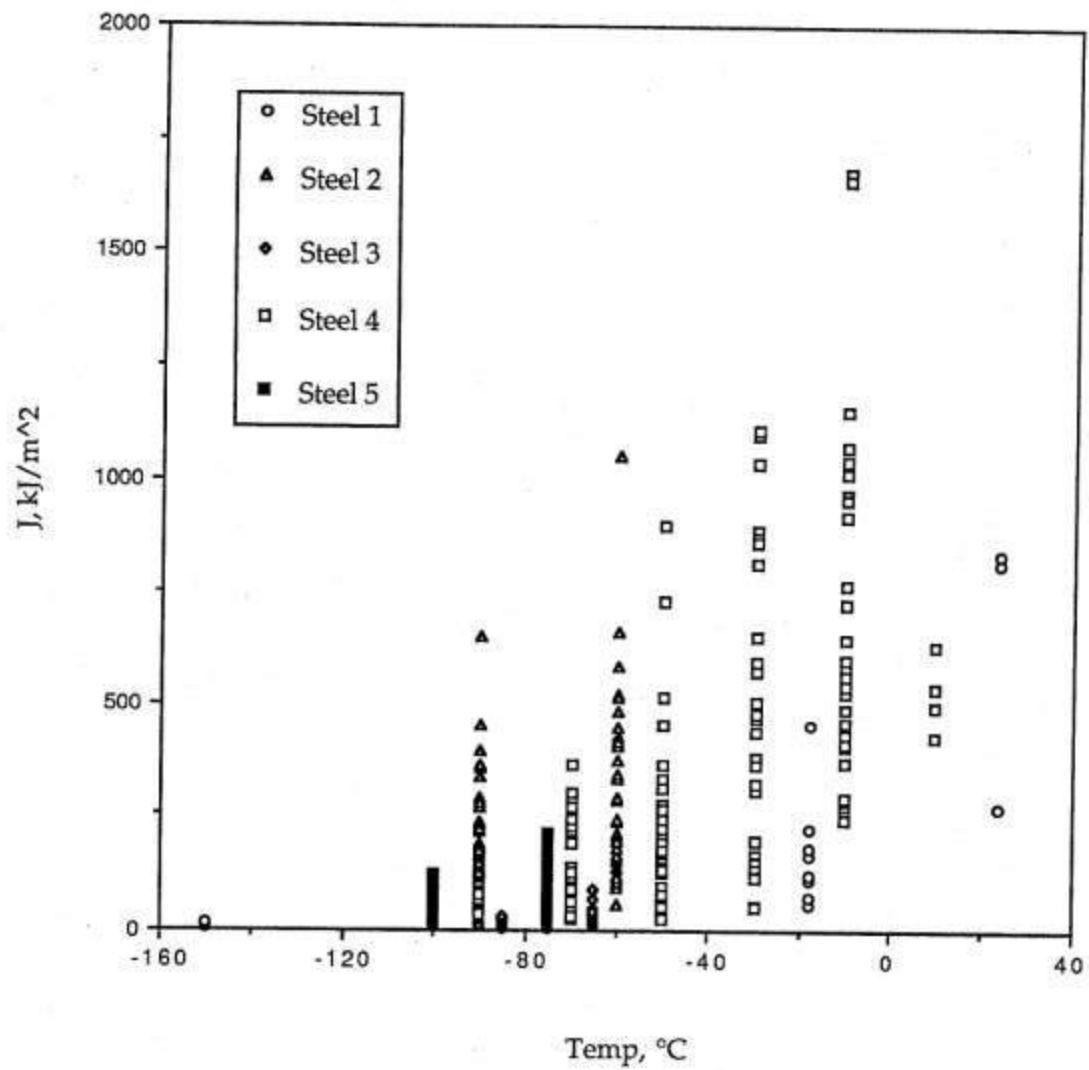
3.2.5.1 *Discussion*—In practice, the value of  $a$  is obtained from procedures for measurement of physical crack size,  $a_p$ , original crack size,  $a_o$ , and effective crack size,  $a_e$ , as appropriate to the situation being considered.

3.2.6 *crack-tip opening displacement* (CTOD),  $\delta$  [ $L$ ],  $n$ —the crack displacement due to elastic and plastic deformation at variously defined locations near the original (prior to an application of load) crack tip.

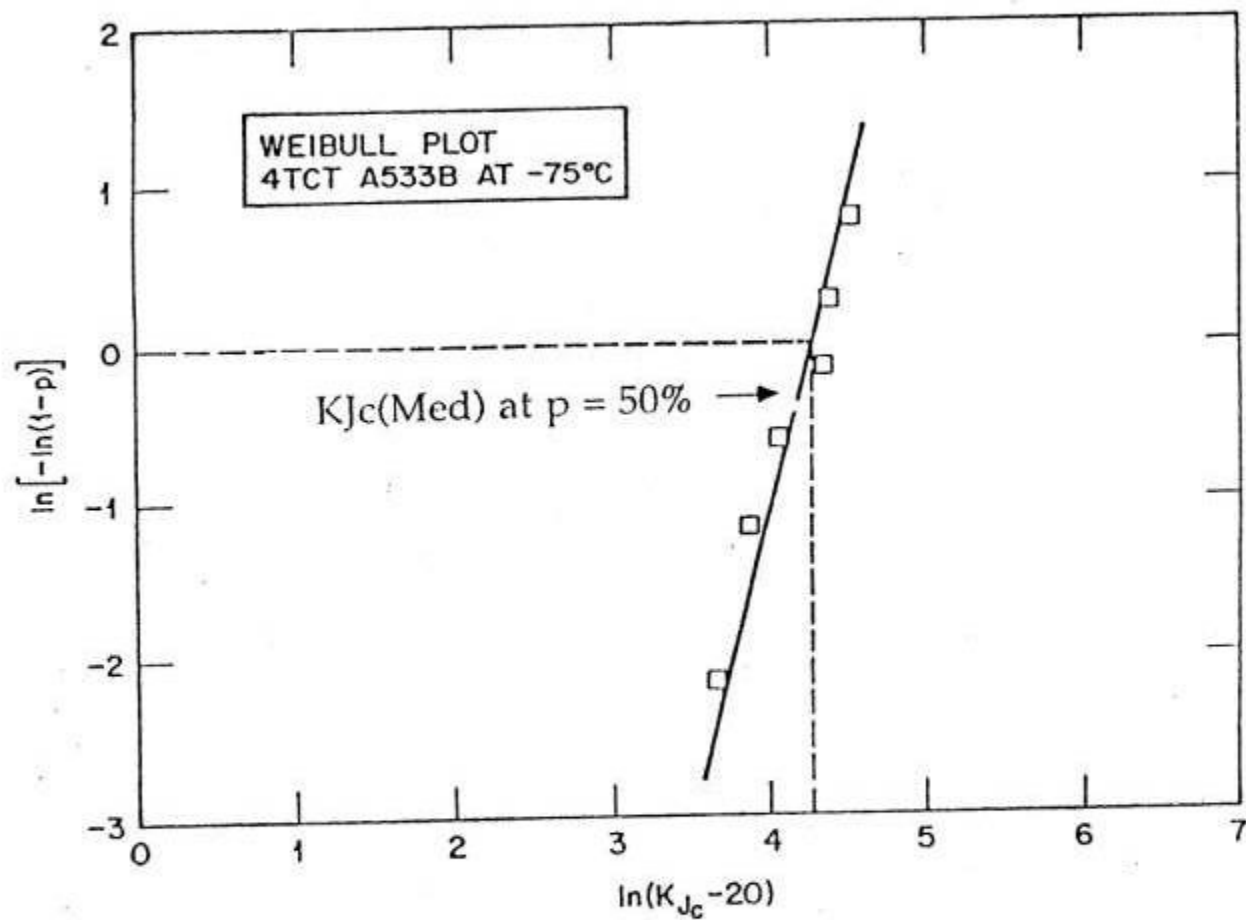
3.2.6.1 *Discussion*—In this test method, CTOD is the displacement of the crack surfaces normal to the original (unloaded) crack plane at the tip of the fatigue precrack,  $a_o$ . In this test method, CTOD is calculated at the original crack length,



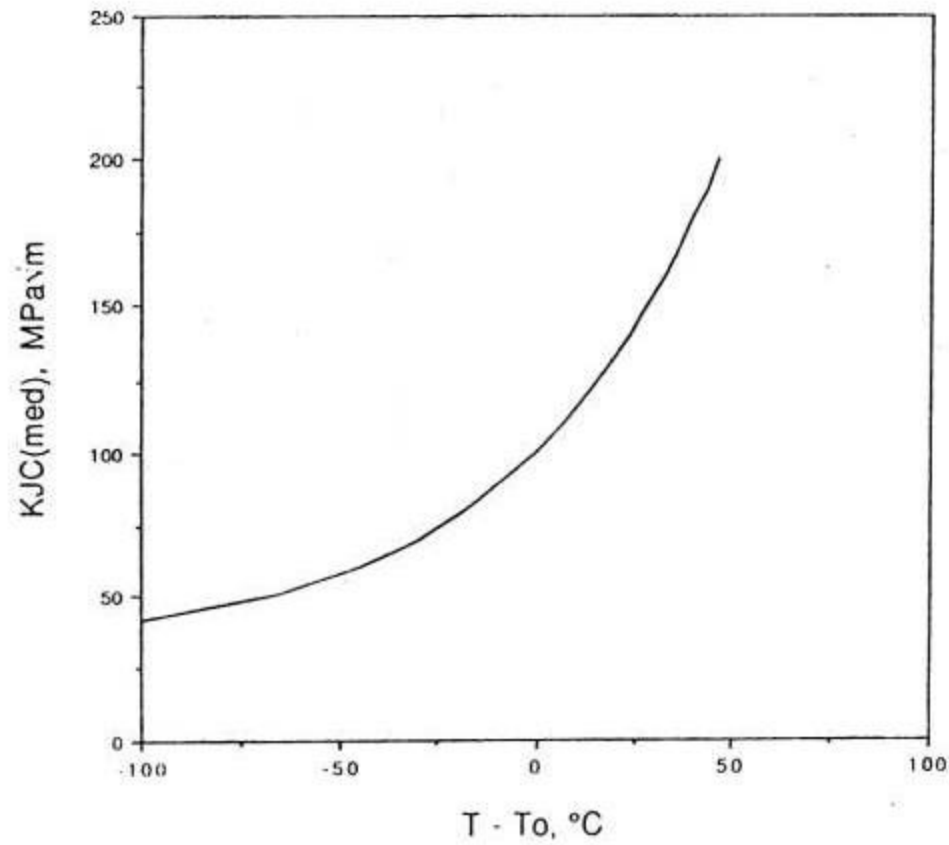
**Fig. 1 - Schematic Showing  
Region of Ductile Fracture**



Transition Toughness Results for five steels



Evaluation of  $K_{Jc}(\text{Med})$  from Weibull Plot



**Master Curve of  $K_{JC}(\text{med})$   
Values in the Transition**

## Transition toughness with Master Curve

1. Determine  $K_{Jc}$  from  $J_c$

$$K_{Jc} = \sqrt{J_c E}$$

2. Adjust to unit size

$$K_{Jc0} = K_{Jcx} \left( \frac{B_x}{B_o} \right)^{\frac{1}{4}}$$

4. Characterize scatter with Weibull statistics

$$1 - P_f = \exp \left[ - \left( \frac{K_{Jc} - 20}{K_o - 20} \right)^4 \right]$$

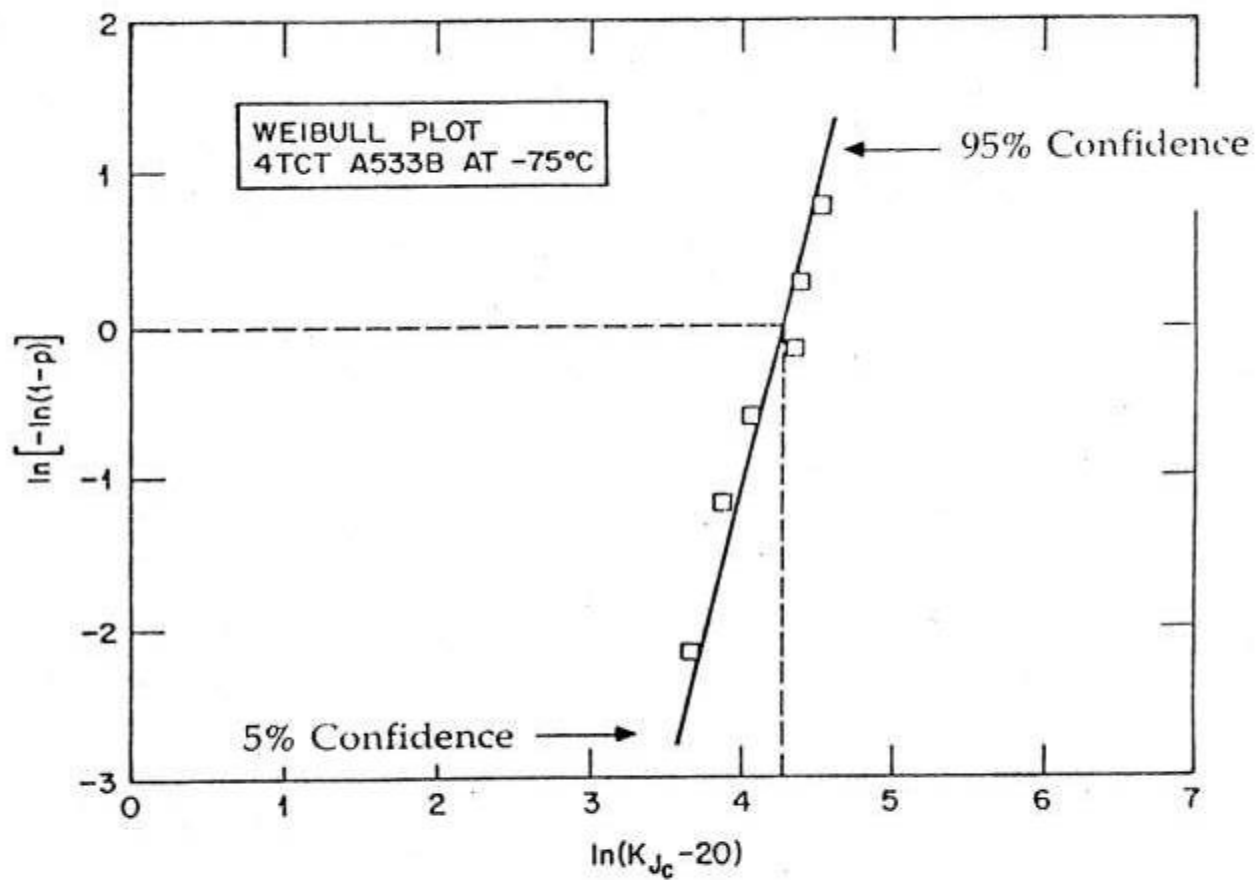
4. Determine the median value,  $K_{Jc(\text{med})}$  at  $P_f = 50 \%$

5. Plot the master curve of

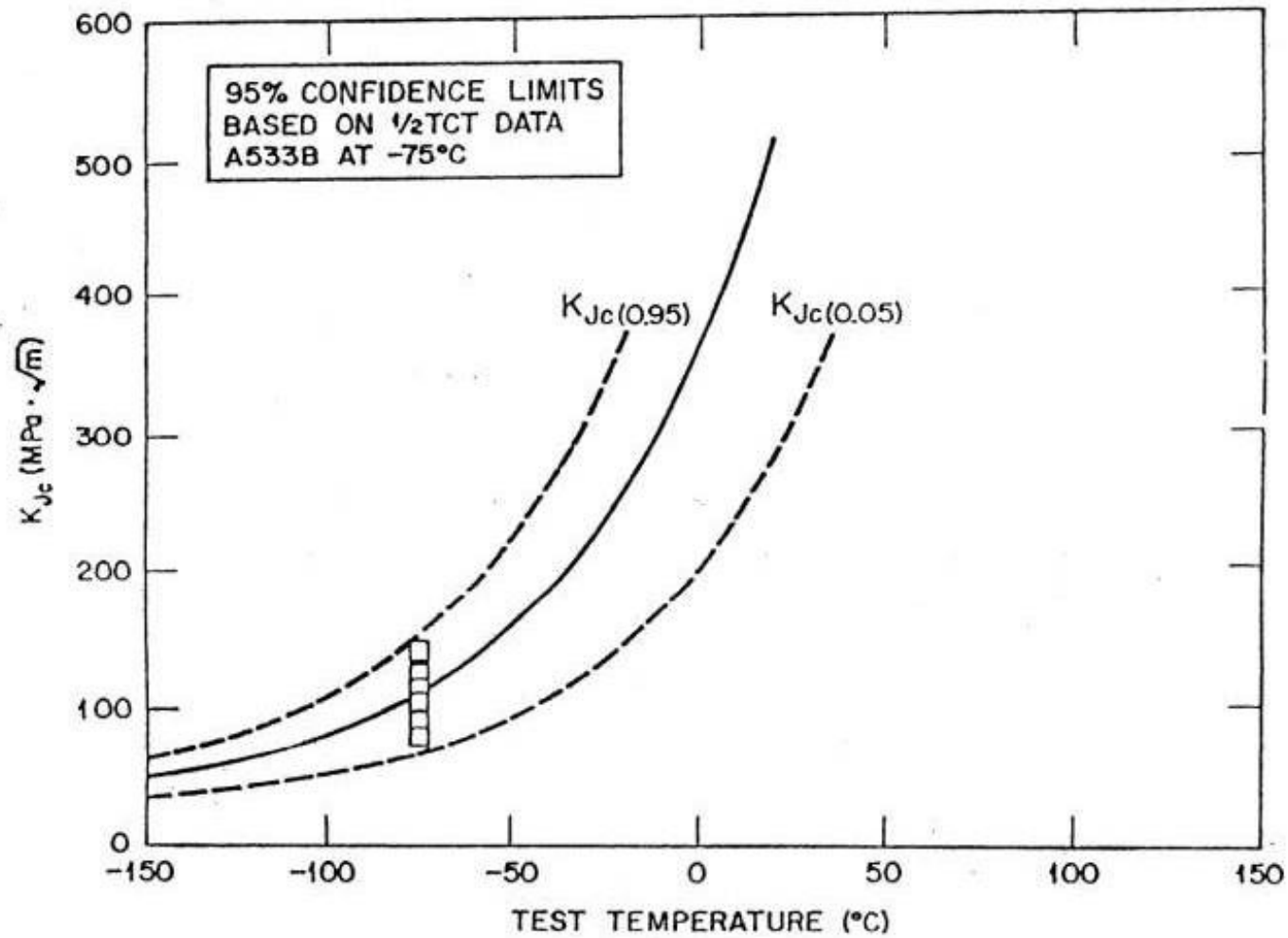
$$K_{Jc(\text{med})} = 30 + 70 \exp[0.019(T - T_o)] \quad (\text{K in MPa}\sqrt{\text{m}})$$

6. Calculate  $T_o$

$$T_o = \left( \frac{1}{0.019} \right) \ln \left[ \frac{K_{Jc(\text{med})} - 30}{70} \right]$$



Evaluation Confidence Limits from Weibull Plot



Master Curve with Confidence Limits

# Standard Test Method for Determination of Reference Temperature, $T_{01}$ , for Ferritic Steels in the Transition Range<sup>1</sup>

This standard is issued under the fixed designation E 1921; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon ( $\epsilon$ ) indicates an editorial change since the last revision or reapproval.

## 1. Scope

1.1 This test method covers the determination of a reference temperature,  $T_{01}$ , which characterizes the fracture toughness of ferritic steels that experience onset of cleavage cracking at elastic, or elastic-plastic  $K_{Ic}$  instabilities, or both. The specific types of ferritic steels (3.2.1) covered are those with yield strength ranging from 275 to 825 MPa (40 to 120 ksi) and weld metals, after stress-relief annealing that have 10 % or less strength mismatch relative to that of the base metal.

1.2 The specimens covered are fatigue precracked single-edge notched bend bars, SE(B), and standard or disk-shaped compact tension specimens, C(T) or DC(T). A range of specimen sizes with proportional dimensions is recommended. The dimension on which the proportionality is based is specimen thickness.

1.3 Requirements are set on specimen size and the number of replicate tests that are needed to establish acceptable characterization of  $K_{Ic}$  data populations.

1.4 The statistical effects of specimen size on  $K_{Ic}$  in the transition range are treated using weakest-link theory (1)<sup>2</sup> applied to a three-parameter Weibull distribution of fracture toughness values. A limit on  $K_{Ic}$  values, relative to the specimen size, is specified to ensure high constraint conditions along the crack front at fracture. For some materials, particularly those with low strain hardening, this limit may not be sufficient to ensure that a single-parameter ( $K_{Ic}$ ) adequately describes the crack-front deformation state (2).

1.5 Statistical methods are employed to predict the transition toughness curve and specified tolerance bounds for IT specimens of the material tested. The standard deviation of the data distribution is a function of Weibull slope and median  $K_{Ic}$ . The procedure for applying this information to the establishment of transition temperature shift determinations and the establishment of tolerance limits is prescribed.

1.6 The fracture toughness evaluation of local brittle zones that are located in heat-affected zones of multipass weldments is not amenable to the statistical methods employed in the present test method.

1.7 This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.

## 2. Referenced Documents

### 2.1 ASTM Standards:

- E 4 Practices for Force Verification of Testing Machines<sup>3</sup>
- E 8M Test Methods for Tension Testing of Metallic Materials (Metric)<sup>3</sup>
- E 74 Practice for Calibration of Force Measuring Instruments for Verifying the Force Indication of Testing Machines<sup>3</sup>
- E 208 Test Method for Conducting Drop-Weight Test to Determine Nil-Ductility Transition Temperature of Ferritic Steels<sup>3</sup>
- E 399 Test Method for Plane-Strain Fracture Toughness of Metallic Materials<sup>3</sup>
- E 436 Test Method for Drop-Weight Tear Tests of Ferritic Steels<sup>3</sup>
- E 561 Practice for R-Curve Determination<sup>3</sup>
- E 812 Test Method for Crack Strength of Slow-Bend, Precracked Charpy Specimens of High-Strength Metallic Materials<sup>3</sup>
- E 813 Test Method for  $J_{Ic}$ , A Measure of Fracture Toughness<sup>3</sup>
- E 1152 Test Method for Determining J-R Curves<sup>3</sup>
- E 1823 Terminology Relating to Fatigue and Fracture Testing<sup>3</sup>

## 3. Terminology

3.1 Terminology given in Terminology E 1823 is applicable to this test method.

### 3.2 Definitions:

3.2.1 *ferritic steel*—carbon and low-alloy steels, and higher alloy steels, with the exception of austenitic stainless, martensitic, and precipitation hardening steels. All ferritic steels have body centered cubic crystal structures that display ductile-to-cleavage transition temperature (see also Test Methods E 208 and E 436).

NOTE 1—This definition is not intended to imply that all of the many

<sup>1</sup> This test method is under the jurisdiction of ASTM Committee E-8 on Fracture and Fatigue and is the direct responsibility of E08.08 on Elastic-Plastic Fracture Mechanics Technology.

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<sup>2</sup> The boldface numbers in parentheses refer to the list of references at the end of this standard.

<sup>3</sup> Annual Book of ASTM Standards, Vol 03.01.

# Latest Transition Toughness Standard

- **ASTM E1921 - 09a Standard Test Method for Determination of Reference Temperature,  $T_0$ , for Ferritic Steels in the Transition Range**

# $da/dN$ vs $\Delta J$

- For cyclic loading that occurs at load levels above a LEFM limit, a  $da/dN$  vs  $\Delta J$  characterization can be used
- There is no standard test method for this